



# Geometric Algebra

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## 3. Applications to 3D dynamics

Dr Chris Doran  
ARM Research

# Recap

Even grade = quaternions

Grade 0  
1 Scalar

1

$$\tilde{\alpha} = \alpha$$

Grade 1  
3 Vectors

$\{\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3\}$

$$\tilde{a} = a$$

Grade 2  
3 Plane / bivector

$\{\mathbf{e}_1\mathbf{e}_2, \mathbf{e}_2\mathbf{e}_3, \mathbf{e}_3\mathbf{e}_1\}$

$$\tilde{B} = -B$$

Grade 3  
1 Volume / trivector

$\mathbf{e}_1\mathbf{e}_2\mathbf{e}_3$

$$\tilde{I} = -I$$

Rotation  $a \mapsto Ra\tilde{R}$

Rotor  $R = e^{-B/2}$

$$aB = a \cdot B + a \wedge B$$

Antisymmetric

Symmetric

# Inner product

Should confirm that rotations do indeed leave inner products invariant

$$\begin{aligned} a' \cdot b' &= (Ra\tilde{R}) \cdot (Rb\tilde{R}) \\ &= \frac{1}{2}(Ra\tilde{R}Rb\tilde{R} + Rb\tilde{R}Ra\tilde{R}) \\ &= \frac{1}{2}R(ab + ba)\tilde{R} \\ &= a \cdot b R\tilde{R} \\ &= a \cdot b \end{aligned}$$

Can also show that rotations do indeed preserve handedness

# Angular momentum

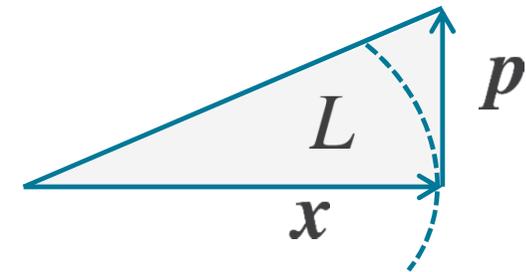
Trajectory  $\mathbf{x}(t)$

Velocity  $\mathbf{v} = \dot{\mathbf{x}}$

Momentum  $\mathbf{p} = m\mathbf{v}$

Force  $\mathbf{f}$

Angular momentum  
measures area  
swept out



Traditional definition  $\mathbf{l} = \mathbf{x} \times \mathbf{p}$

An 'axial' vector instead of  
a 'polar' vector

Much better to treat angular  
momentum as a bivector

$$L = \mathbf{x} \wedge \mathbf{p}$$

# Torque

Differentiate the  
angular momentum

$$\dot{L} = \mathbf{v} \wedge (m\mathbf{v}) + \mathbf{x} \wedge (\dot{\mathbf{p}}) = \mathbf{x} \wedge \mathbf{f}$$

Define the torque bivector  $N = \mathbf{x} \wedge \mathbf{f}$

Define  $\mathbf{x} = r\hat{\mathbf{x}}$

Differentiate  $\dot{\mathbf{x}} = \dot{r}\hat{\mathbf{x}} + r\dot{\hat{\mathbf{x}}}$

$$\begin{aligned} \text{So } L &= m\mathbf{x} \wedge (\dot{r}\hat{\mathbf{x}} + r\dot{\hat{\mathbf{x}}}) \\ &= mr\hat{\mathbf{x}} \wedge (\dot{r}\hat{\mathbf{x}} + r\dot{\hat{\mathbf{x}}}) \\ &= mr^2 \hat{\mathbf{x}} \wedge \dot{\hat{\mathbf{x}}} \end{aligned}$$

But  $\hat{\mathbf{x}}^2 = 1$

$$0 = \frac{d}{dt}(\hat{\mathbf{x}}^2) = 2\hat{\mathbf{x}} \cdot \dot{\hat{\mathbf{x}}}$$

$$L = -mr^2 \dot{\hat{\mathbf{x}}} \hat{\mathbf{x}}$$

# Inverse-square force

$$m\ddot{\mathbf{x}} = -\frac{k}{r^2}\hat{\mathbf{x}} = -\frac{k}{r^3}\mathbf{x}$$

Simple to see that torque vanishes, so  $L$  is conserved. This is one of two conserved vectors.

$$\begin{aligned} L\dot{\mathbf{v}} &= -\frac{k}{mr^2}L\hat{\mathbf{x}} \\ &= -k\hat{\mathbf{x}}\dot{\mathbf{x}}\hat{\mathbf{x}} = k\dot{\hat{\mathbf{x}}} \end{aligned}$$

So 
$$\frac{d}{dt}(L\mathbf{v} - k\hat{\mathbf{x}}) = 0$$

Define the eccentricity vector

$$L\mathbf{v} = k(\hat{\mathbf{x}} + \mathbf{e})$$

Forming scalar part of  $L\mathbf{v}\cdot\hat{\mathbf{x}}$  find

$$r = \frac{l^2}{km(1 + \mathbf{e}\cdot\hat{\mathbf{x}})}$$

# Rotating frames



Frames related by a time dependent rotor  $\mathbf{f}_k(t) = R(t)\mathbf{e}_k\tilde{R}(t)$

Traditional definition of angular velocity  $\dot{\mathbf{f}}_k = \boldsymbol{\omega} \times \mathbf{f}_k$

Replace this with  
a bivector

$$\dot{\mathbf{f}}_k = \dot{R}\mathbf{e}_k\tilde{R} + R\mathbf{e}_k\dot{\tilde{R}} = \dot{R}\tilde{R}\mathbf{f}_k + \mathbf{f}_k R\dot{\tilde{R}}$$

Need to understand the rotor derivative, starting from  $R\tilde{R} = 1$

# Rotor derivatives

$$0 = \frac{d}{dt}(R\tilde{R}) = \dot{R}\tilde{R} + R\dot{\tilde{R}}$$

$$\dot{R}\tilde{R} = -R\dot{\tilde{R}} = -(\dot{R}\tilde{R})^\sim$$

An even object equal to minus it's own reverse, so must be a bivector

$$2\dot{R}\tilde{R} = -\Omega$$

$$\dot{R} = -\frac{1}{2}\Omega R$$

Lie group
Lie algebra

$$\dot{f}_k = \dot{R}\tilde{R}f_k - f_k\dot{R}\tilde{R} = f_k \cdot \Omega$$

As expected, angular momentum now a bivector

$$\Omega = I\omega$$

# Constant angular velocity

$$\dot{R} = -\frac{1}{2}\Omega R$$

Integrates easily in the case of constant Omega  $R = e^{-\Omega t/2} R_0$

$$f_k(t) = e^{-\Omega t/2} \underline{R_0 e_k \tilde{R}_0} e^{\Omega t/2}$$

Fixed frame at  $t=0$

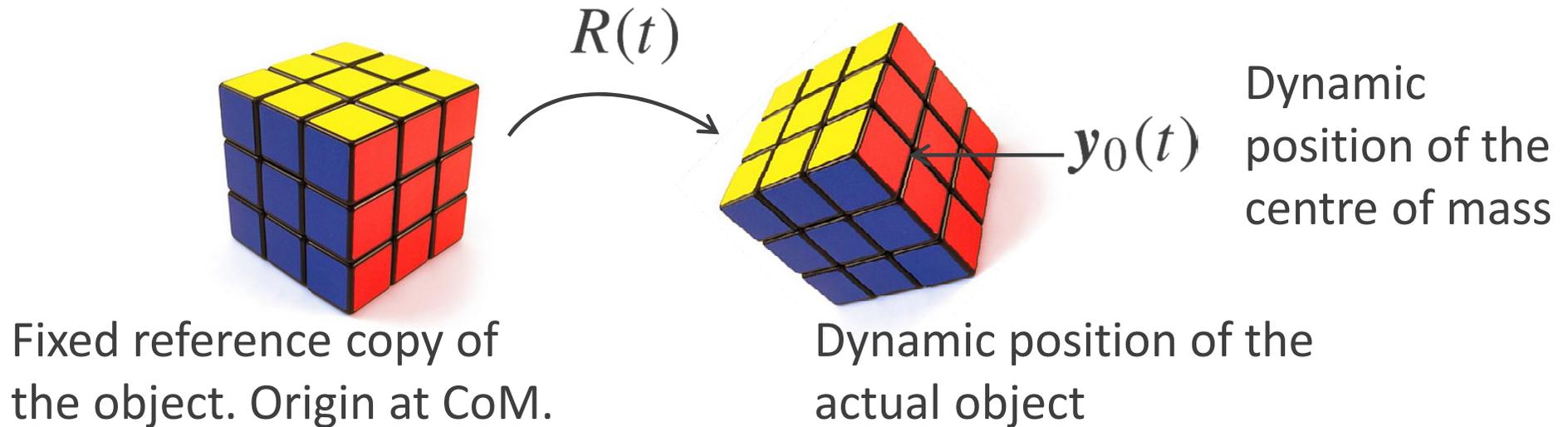
Example – motion around

a fixed z axis:  $\Omega = -\omega I e_3 = -\omega e_1 e_2$

$$R_0 = 1$$



# Rigid-body dynamics



- $\mathbf{x}_i$  Constant position vector in the reference copy
- $\mathbf{y}_i(t)$  Position of the equivalent point in space

$$\mathbf{y}_i(t) = R(t)\mathbf{x}_i\tilde{R}(t) + \mathbf{y}_0(t)$$

# Velocity and momentum

$$\dot{R} = -\frac{1}{2}\Omega R = -\frac{1}{2}R\Omega_B$$

Spatial bivector

Body bivector

$$\Omega = R\Omega_B\tilde{R}$$

$$\begin{aligned}\mathbf{v}(t) &= \dot{R}\mathbf{x}\tilde{R} + R\mathbf{x}\dot{\tilde{R}} + \dot{\mathbf{y}}_0 \\ &= R\mathbf{x}\cdot\Omega_B\tilde{R} + \mathbf{v}_0\end{aligned}$$

True for all points. Have  
dropped the index

Use continuum approximation  
Centre of mass defined by

$$\int d^3x \rho \mathbf{x} = 0$$

Momentum given by

$$\begin{aligned}\int d^3x \rho \mathbf{v} &= \int d^3x \rho (R\mathbf{x}\cdot\Omega_B\tilde{R} + \mathbf{v}_0) \\ &= M\mathbf{v}_0\end{aligned}$$

# Angular momentum

Need the angular momentum of the body about its instantaneous centre of mass

$$\begin{aligned}
 L &= \int d^3x \rho(\mathbf{y} - \mathbf{y}_0) \wedge \mathbf{v} \\
 &= \int d^3x \rho(R\mathbf{x}\tilde{R}) \wedge (R\mathbf{x} \cdot \Omega_B \tilde{R} + \mathbf{v}_0) \\
 &= R \left( \int d^3x \rho \mathbf{x} \wedge (\mathbf{x} \cdot \Omega_B) \right) \tilde{R}
 \end{aligned}$$

Fixed function of the angular velocity bivector

Define the Inertia Tensor

$$\mathcal{I}(B) = \int d^3x \rho \mathbf{x} \wedge (\mathbf{x} \cdot B)$$

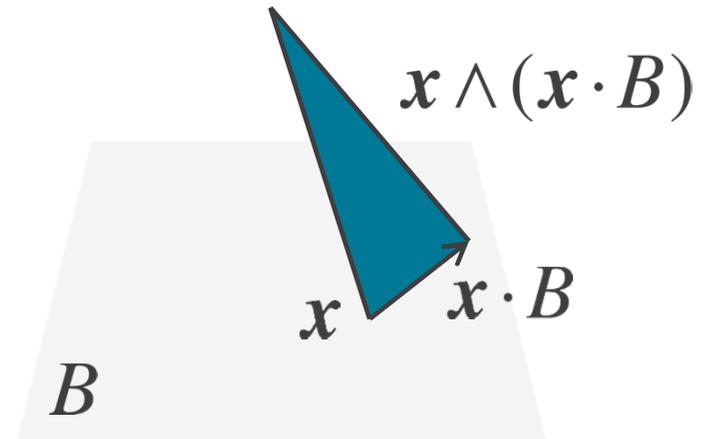
This is a linear, symmetric function

$$\mathcal{I}(\lambda A + \mu B) = \lambda \mathcal{I}(A) + \mu \mathcal{I}(B)$$

$$\langle A \mathcal{I}(B) \rangle = \langle \mathcal{I}(A) B \rangle$$

# The inertia tensor

Inertia tensor input is the bivector  $B$ .  
Body rotates about centre of mass in the  $B$  plane.



Angular momentum of the point is  $\mathbf{x} \wedge (\rho \mathbf{x} \cdot B)$

Back rotate the angular velocity to the reference copy  $\Omega_B = \tilde{R} \Omega R$

Find angular momentum in the reference copy  $\mathcal{I}(\Omega_B)$

Rotate the body angular momentum forward  
to the spatial copy of the body

$$L = R \mathcal{I}(\Omega_B) \tilde{R}$$

# Equations of motion

$$\begin{aligned}
 \dot{L} &= \dot{R}\mathcal{I}(\Omega_B)\tilde{R} + R\mathcal{I}(\Omega_B)\dot{\tilde{R}} + R\mathcal{I}(\dot{\Omega}_B)\tilde{R} \\
 &= R[\mathcal{I}(\dot{\Omega}_B) - \frac{1}{2}\Omega_B\mathcal{I}(\Omega_B) + \frac{1}{2}\mathcal{I}(\Omega_B)\Omega_B]\tilde{R} \\
 &= R[\mathcal{I}(\dot{\Omega}_B) - \Omega_B \times \mathcal{I}(\Omega_B)]\tilde{R}
 \end{aligned}$$

From now on, use the cross symbol for the commutator product

$$A \times B = \frac{1}{2}(AB - BA)$$

The commutator of two bivectors is a third bivector

Introduce the principal axes and principal moments of inertia

$$\mathcal{I}(I\mathbf{e}_k) = i_k I\mathbf{e}_k \quad \text{No sum}$$

Symmetric nature of inertia tensor guarantees these exist

# Equations of motion

$$N = R[\mathcal{I}(\dot{\Omega}_B) - \Omega_B \times \mathcal{I}(\Omega_B)]\tilde{R}$$

$$\Omega = \sum_{k=1}^3 \omega_k I f_k$$

Objects  
expressed in  
terms of the  
principal axes

$$\Omega_B = \sum_{k=1}^3 \omega_k I e_k$$

$$L = \sum_{k=1}^3 i_k \omega_k I f_k$$

Inserting these in the above  
equation recover the famous  
Euler equations

$$i_1 \dot{\omega}_1 - \omega_2 \omega_3 (i_2 - i_3) = N_1$$

$$i_2 \dot{\omega}_2 - \omega_3 \omega_1 (i_3 - i_1) = N_2$$

$$i_3 \dot{\omega}_3 - \omega_1 \omega_2 (i_1 - i_2) = N_3$$

# Kinetic energy

$$T = \frac{1}{2} \int d^3x \rho (R \mathbf{x} \cdot \boldsymbol{\Omega}_B \tilde{R})^2 = \frac{1}{2} \int d^3x \rho (\mathbf{x} \cdot \boldsymbol{\Omega}_B)^2$$

Use this  
rearrangement

$$(\mathbf{x} \cdot \boldsymbol{\Omega}_B)^2 = \langle \mathbf{x} \cdot \boldsymbol{\Omega}_B \mathbf{x} \boldsymbol{\Omega}_B \rangle = -\boldsymbol{\Omega}_B \cdot (\mathbf{x} \wedge (\mathbf{x} \cdot \boldsymbol{\Omega}_B))$$

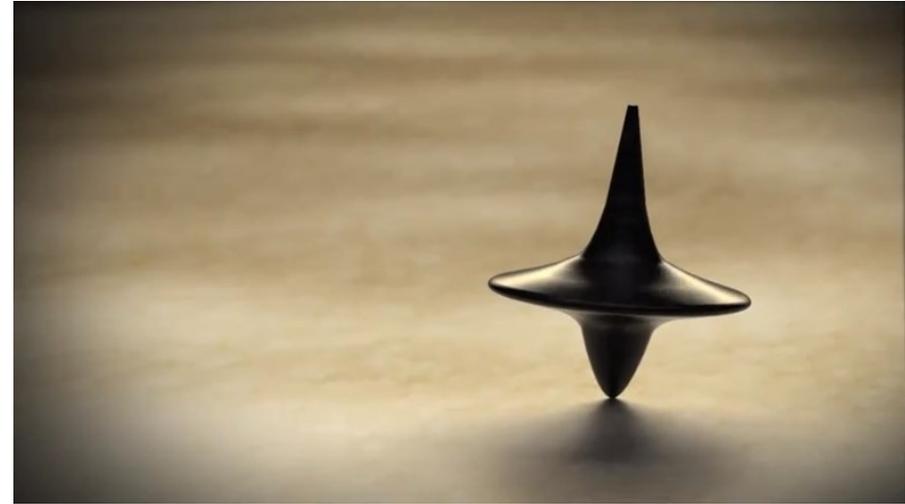
$$T = -\frac{1}{2} \boldsymbol{\Omega}_B \cdot \mathcal{I}(\boldsymbol{\Omega}_B) = \frac{1}{2} \tilde{\boldsymbol{\Omega}}_B \cdot \mathcal{I}(\boldsymbol{\Omega}_B)$$

In terms of components

$$T = \frac{1}{2} \sum_{k=1}^3 i_k \omega_k^2 = \frac{1}{2} \sum_{k=1}^3 \frac{L_k^2}{i_k}$$

# Symmetric top

Body with a symmetry axis aligned with the 3 direction, so  $i_1 = i_2$



Action of the inertia tensor is

$$\begin{aligned}\mathcal{I}(\Omega_B) &= i_1\omega_1\mathbf{e}_2\mathbf{e}_3 + i_1\omega_2\mathbf{e}_3\mathbf{e}_1 + i_3\omega_3\mathbf{e}_1\mathbf{e}_2 \\ &= i_1\Omega_B + (i_3 - i_1)\omega_3 I\mathbf{e}_3\end{aligned}$$

Third Euler equation reduces to  $i_3\dot{\omega}_3 = 0$

Can now write 
$$\Omega = R\Omega_B\tilde{R} = \frac{1}{i_1}L + \frac{i_1 - i_3}{i_1}\omega_3 R I \mathbf{e}_3 \tilde{R}$$

## Symmetric top

$$\dot{R} = -\frac{1}{2}\Omega R = -\frac{1}{2i_1}(LR + R(i_1 - i_3)\omega_3 I e_3)$$

Define the two  
constant bivectors

$$\Omega_l = \frac{1}{i_1}L, \quad \Omega_r = \omega_3 \frac{i_1 - i_3}{i_1} I e_3$$

Rotor equation is now  $\dot{R} = -\frac{1}{2}\Omega_l R - \frac{1}{2}R\Omega_r$

$$R(t) = \exp\left(-\frac{1}{2}\Omega_l t\right) R_0 \exp\left(-\frac{1}{2}\Omega_r t\right)$$

Fully describes the motion

Internal rotation gives precession

Fixed rotor defines attitude at  $t=0$

Final rotation defines attitude in  
space

# Resources

[geometry.mrao.cam.ac.uk](http://geometry.mrao.cam.ac.uk)  
[chris.doran@arm.com](mailto:chris.doran@arm.com)  
[cjld1@cam.ac.uk](mailto:cjld1@cam.ac.uk)  
[@chrisjldoran](https://twitter.com/chrisjldoran)  
[#geometricalgebra](https://twitter.com/#geometricalgebra)  
[github.com/ga](https://github.com/ga)

